

# Improved Wear Resistance of Martensitic Stainless Steel

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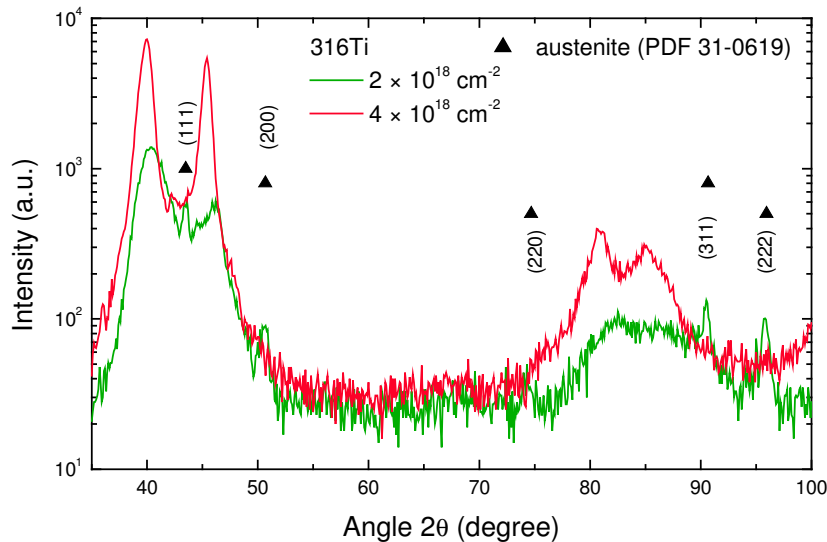
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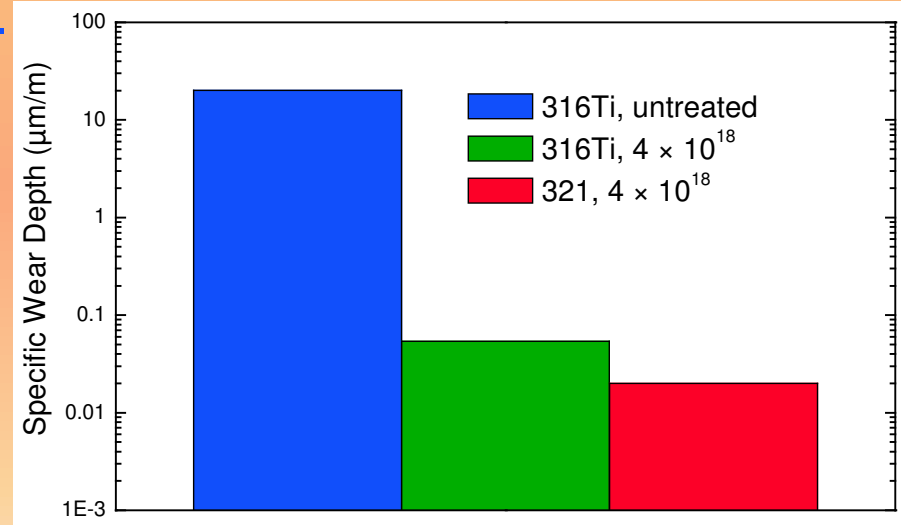
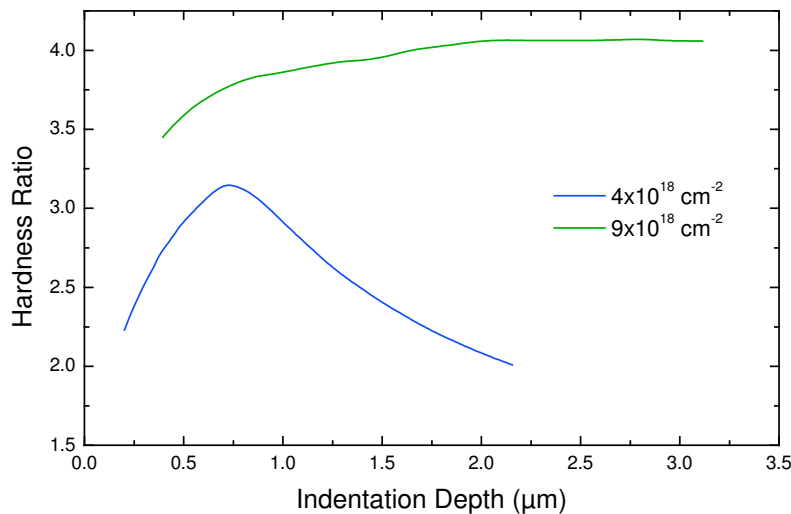
# Motivation



# Austenitic Stainless Steel



- Formation of expanded austenite characterised by anisotropic lattice expansion and concentration dependent diffusion coefficient.
- Hardness increases to 1000 - 1200 HV after nitrogen insertion (PIII, low energy implantation or plasma nitriding).
- Large wear reduction of 2 - 3 orders of magnitude.



## Martensitic Steel

Very good wear resistance

Moderately good corrosion resistance

### Applications

Turbine blades, tools, knives

Bearings, structural aircraft parts

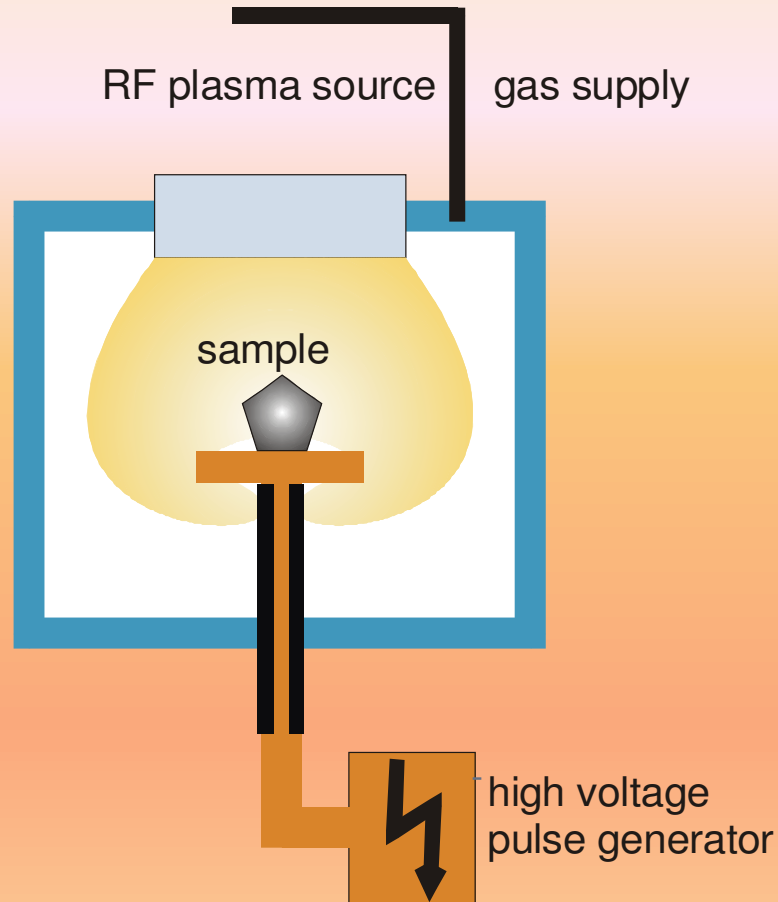
Orthopaedic surgery, bone saws

Dental surgery

***Possibility of hardening with energetic nitrogen implantation?***



## Experiment



### PIII into martensitic stainless steel

1.4542 (X5CrNiCuNb17.4), 1.4021 (X20Cr13), 1.4034 (X46Cr13), 1.4057 (X20CrNi17.2), 1.4104 (X12CrMoS17)

Pulse voltage 10 and 25 kV,

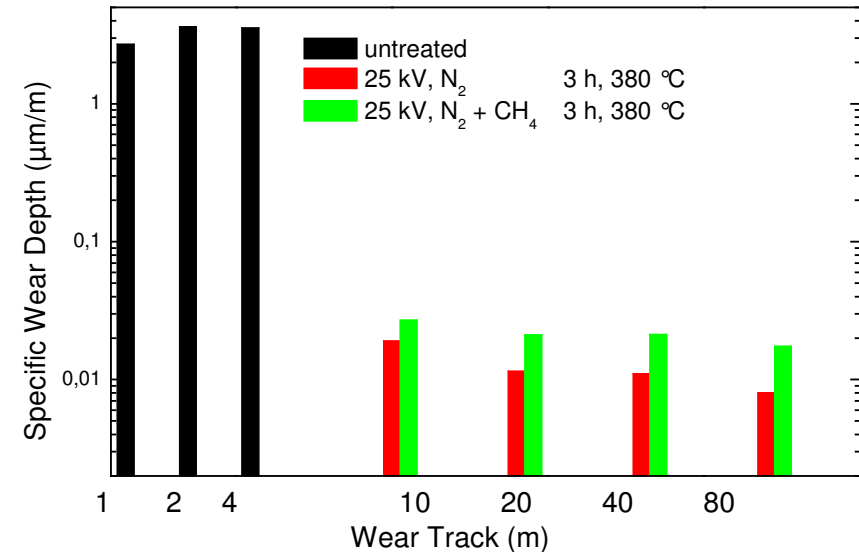
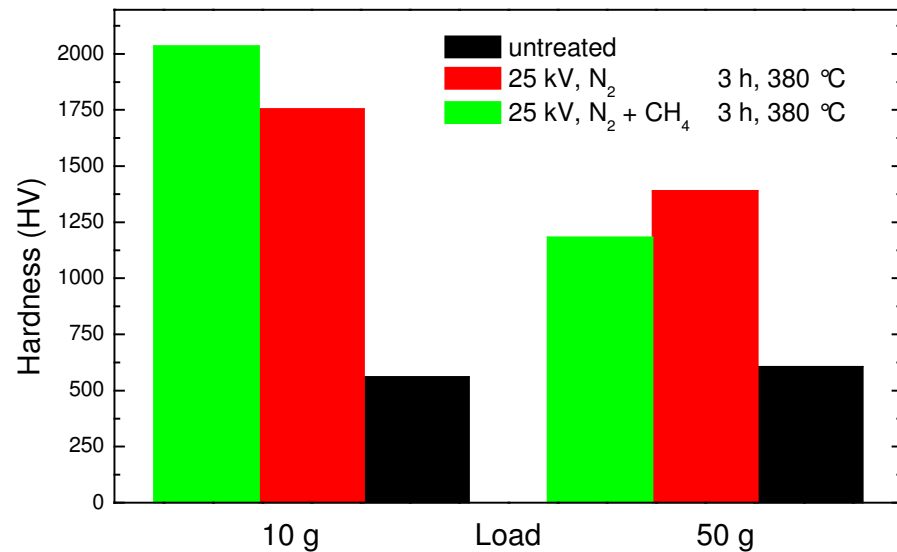
Nitrogen or nitrogen/methane atmosphere

380 °C°, 1 - 6 h implantation time.

Analysis: XRD + glow discharge optical spectroscopy (GDOS).

Hardness measurements, wear resistance measurements

## Martensitic Steel Grade 1.4542



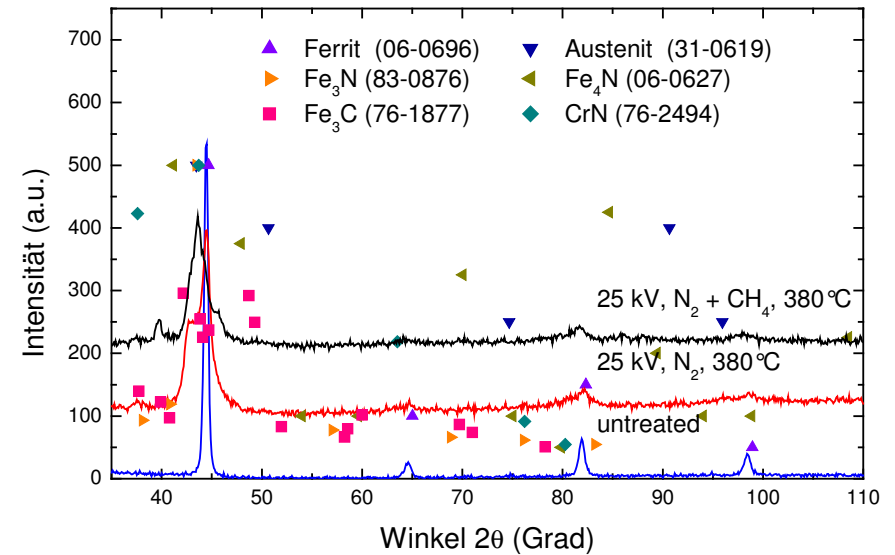
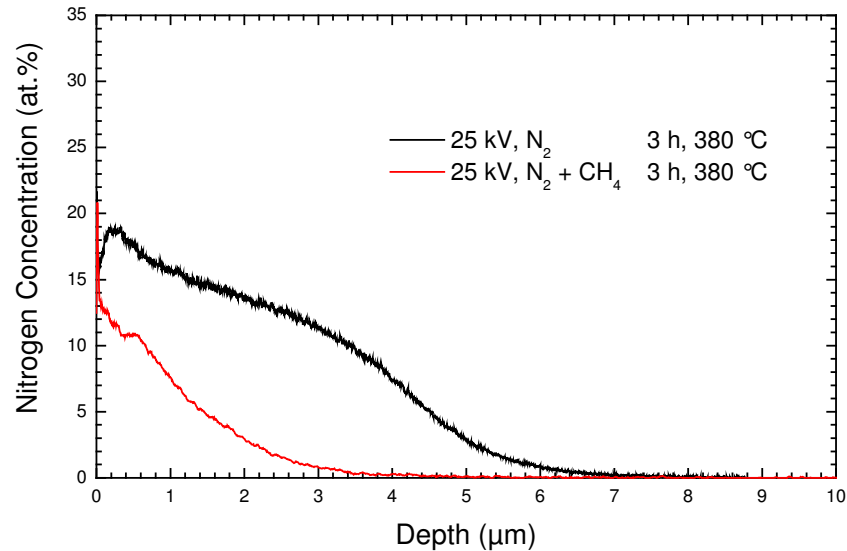
No hardness variation with load for non-implanted sample

Increased hardness up to 2000 HV, significantly decreasing for higher load, thus indicating a layered system

Highly reduced wear by two orders of magnitude (contact pressure 1.0 GPa, low speed)

No breakthrough through layer even up to 80 or 400 m wear track length

# Martensite Steel Grade 1.4542



Fast nitrogen diffusion (slowed by additional carbon)

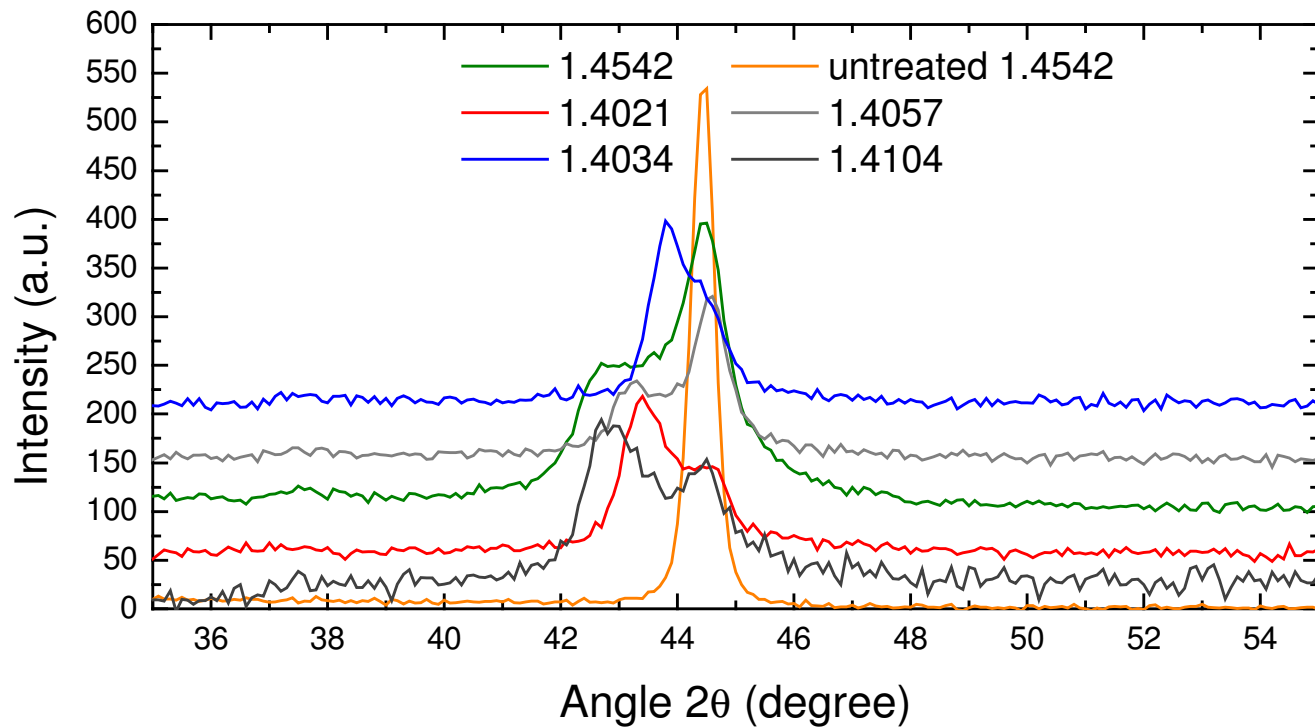
Concentration dependent diffusion constant (deviation from erfc shape)

Formation of “expanded martensite”

Anisotropic lattice expansion



## XRD – different steel grades



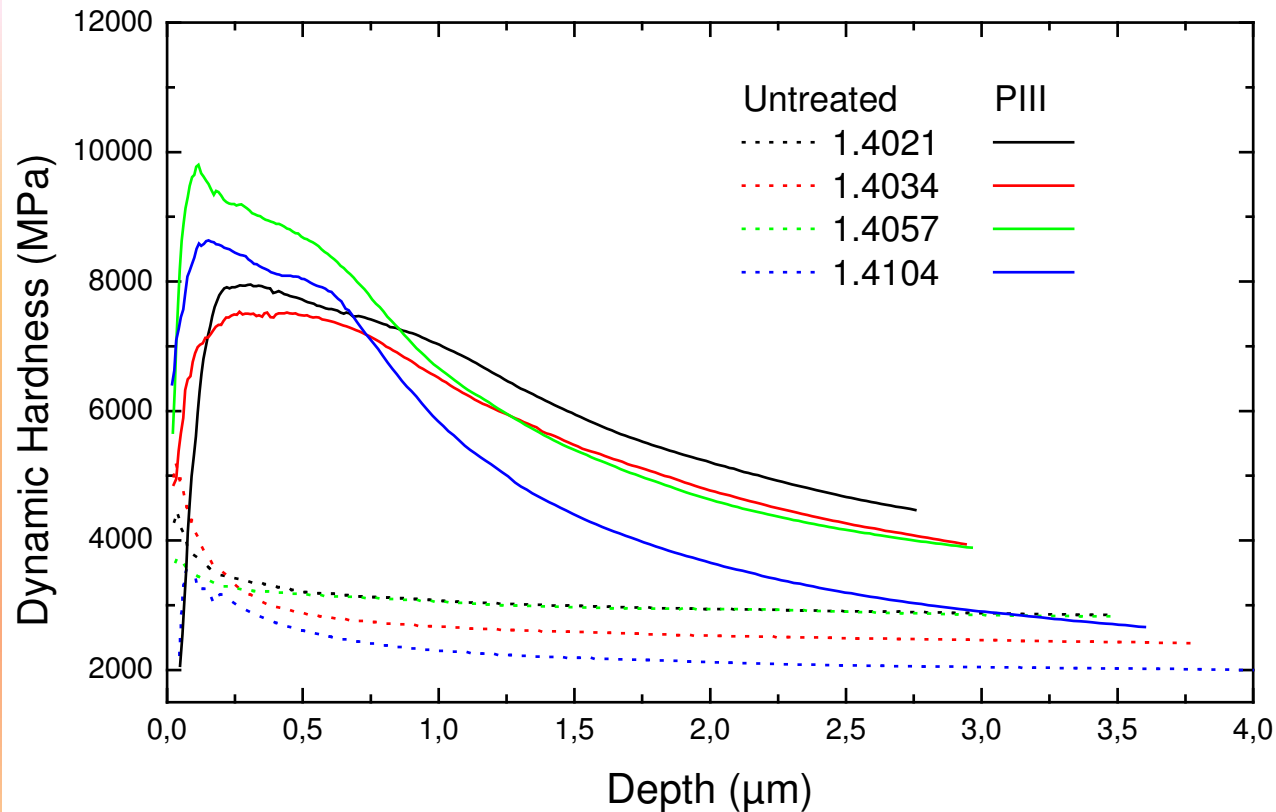
Expanded lattice after nitrogen PIII for all investigated grades

Lattice expansion depends on steel grades

No other phases in XRD spectra (range 30° - 90°)

Layer thickness varying between steel grades at identical treatments (smallest for 1.4542)

## Hardness- different steel grades

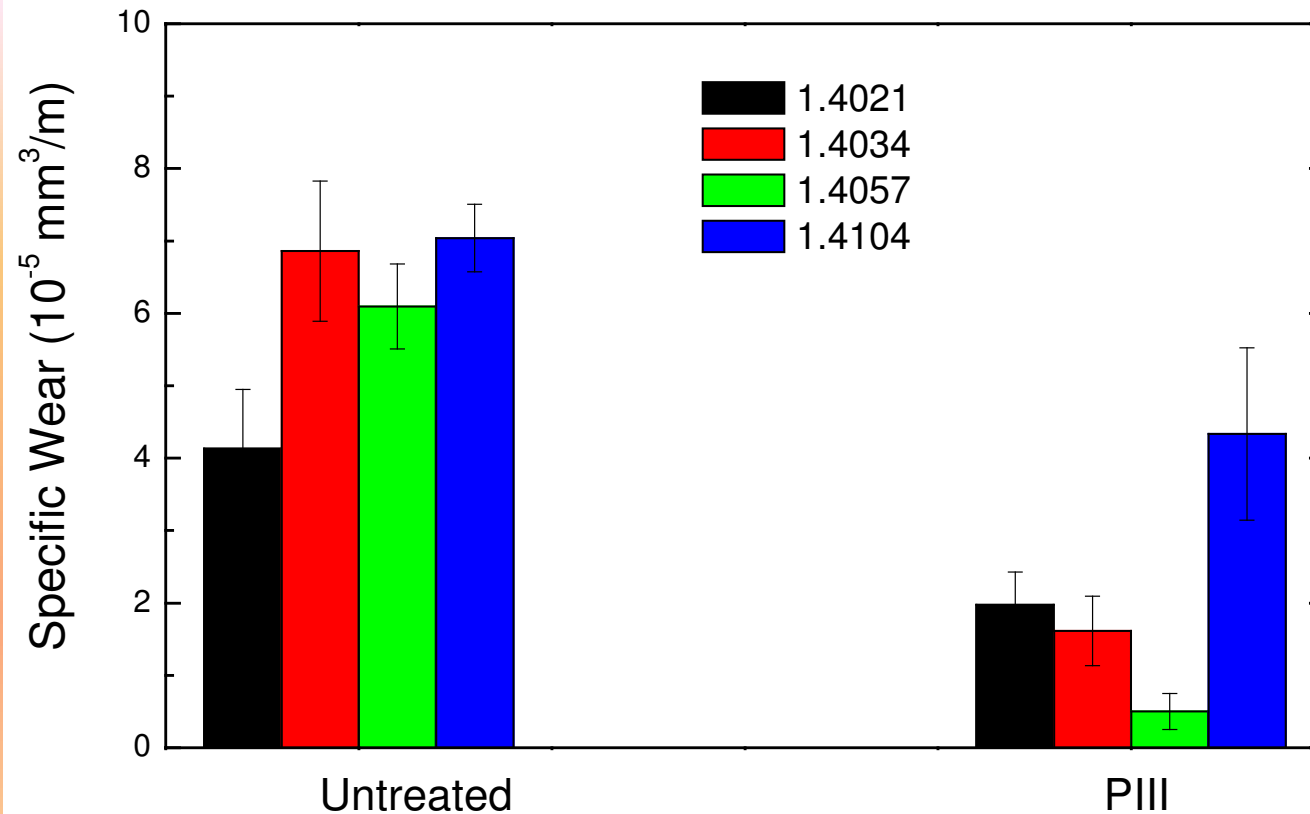


Significantly improved hardness for all steel grades up to 9810 MPa ( $\equiv$  1000 HV)

Absolute and relative increase depends on steel grade / chemical composition

No correction for elastic deformation, i.e. corrected values are about 15 - 20% higher

## Wear resistance – different steel grades



Experimental conditions: contact pressure 1.4 GPa, high speed

High variability in wear reduction

Not identical wear mode as for the high performance steel 1.4542

## Discussion

### Lattice expansion of steel after interstitial atom insertion at 330 – 400 °C

Formation of expanded austenite/martensite independent of

**Chemical nature of ions** (nitrogen or carbon)

no formation of nitride or carbide detected

**Energy range of ions** (method of nitriding)

austenites  $\checkmark$  / martensites (??)

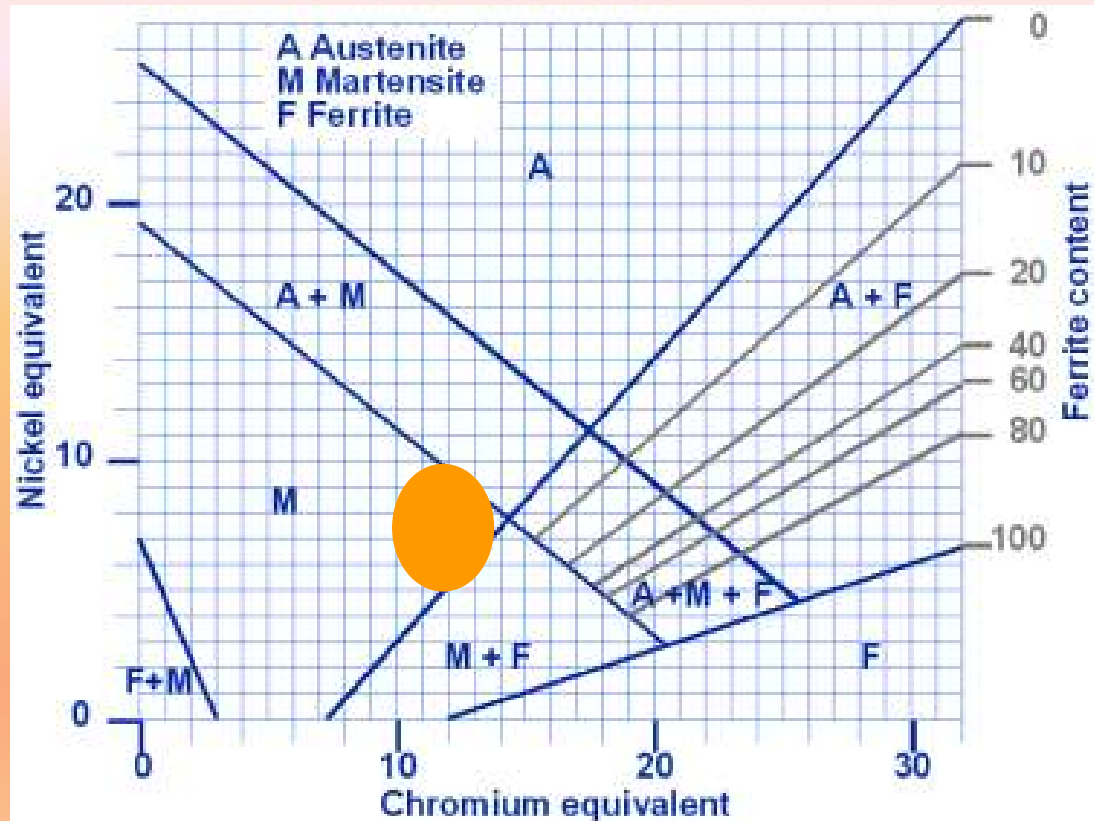
**Composition of Steel**

*Apparently no access to investigate and identify the mechanism*

No chemical path!

Metallurgical path?

## Schäfflerdiagramm



⇒ *Formation of expanded martensite not related with metallurgical phase transition!*

$$Ni = 30(C+N) + 0.5 Mn + Ni + 0.5 (Cu+Co)$$

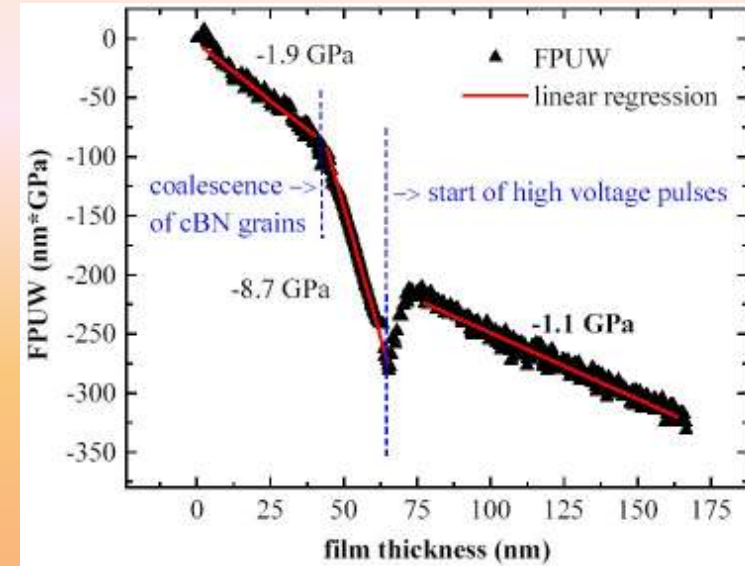
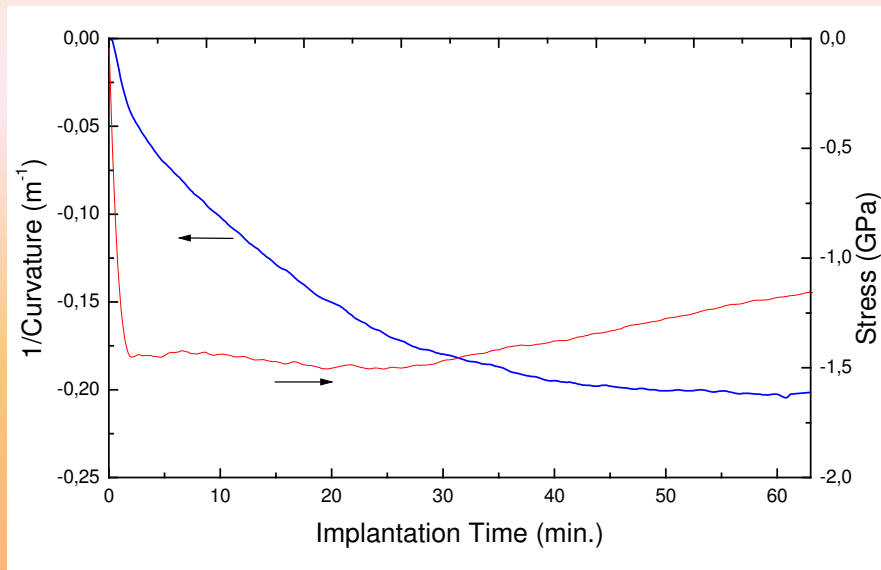
$$Cr = 1.5Si + Cr + Mo + 2Ti + 0.5 Nb$$

Introduction of nitrogen into steel should lead to increase of nickel equivalent

However, no austenitic phase found in XRD spectra even for high-Ni alloys

⇒ Expected phase transition from martensite to austenite is not observed

## Discussion



S. Sienz, S. Mändl, B. Rauschenbach, Surf. Coat. Technol. **156**, 185 (2002).

B. Abendroth, A. Kolitsch, Annual FZR Report 2002

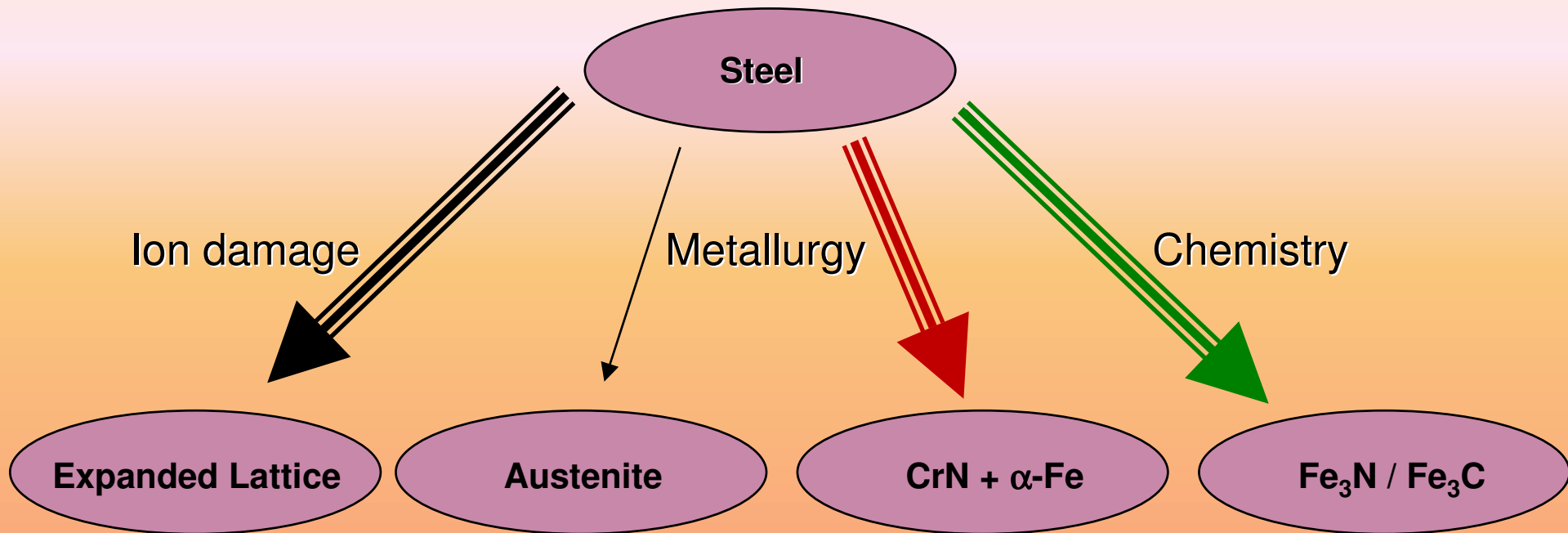
Very fast increase of stress in the beginning of austenite nitriding

Accumulation of stress for BN leads to phase transition h-BN to c-BN

Same cause for austenite and BN: accommodation of stress necessary for transition?

**However: Inward ⇔ Outward growth**

## Discussion & Conclusions



Additional reaction path: influence of deposited energy

Low energy limit for expanded martensite formation!

Temperature dependence:  $< 330\text{ °C} < 400\text{ °C} <$

Thermal activation energy, reaction enthalpy, potential barrier?

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